EL804518676US

EXPRESS MAIL LABEL NO.: DATE: December 12, 2001

FORM PTO (REV 11-200		ATTORNEY'S DOCKET NUMBER			
,	RANSMITTAL LETTER TO THE UNITED STATES	LAGROTH-028			
	DESIGNATED/ELECTED OFFICE (DO/EO/US)	U.S APPLICATION NO. (If known, see 37 CFR 1.5)			
INITEDNI	CONCERNING A FILING UNDER 35 U.S.C. 371				
INTERN	ATIONAL APPLICATION NO. INTERNATIONAL FILING DATES PCT/SE00/01257 15 June 2000	PRIORITY DATE CLAIMED 17 June 1999			
TITLE C	FINVENTION METHOD AND MEANS FOR MEASURING STREET				
APPLIC	ANT(S) FOR DO/EO/US Hans-Olof Backlund				
Applicant	Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information:				
1. x	This is a FIRST submission of items concerning a filing under 35 U.S.C.	371.			
2.	This is a SECOND or SUBSEQUENT submission of items concerning a				
3. x	3. X This is an express request to begin national examination procedures (35 U.S.C. 371 (f)). The submission must include items (5), (6), (9) and (21) indicated below.				
4. x	The US has been elected by the expiration of 19 months from the priority	date (PCT Article 31).			
5. x	A copy of the International Application as filed (35 U.S.C 371 (c)(2))	,			
a.	is attached hereto (required only if not communicated by the Internati	onal Bureau).			
b.	x has been communicated by the International Bureau.				
c.	is not required, as the application was filed in the United States Receiving Office (RO/US).				
6.	An English language translation of the International Application as filed (35 U.S.C. 371 (c)(2)).				
a	is attached hereto.				
b.	has been previously submitted under 35 U.S.C. 154(d)(4).				
7. x	Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371 (c)(3))				
a.	are attached hereto (required only if not communicated by the International Bureau).				
b.	have been communicated by the International Bureau.				
c.	have not been made; however, the time limit for making such amendments has NOT expired.				
d	x have not been made and will not be made.				
8.	An English language translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371 (c)(3)).				
9. x	An oath or declaration of the inventor(s) (35 U.S.C. 371 (c)(4)). (Executed)				
10.	An English language translation of the annexes to the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371 (c)(5)).				
Items 11 to 20 below concern document(s) or information included:					
11. x	. X An Information Disclosure Statement under 37 CFR 1.97 and 1.98. w/PTO-1449, 2 references				
12. x	An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included.				
13. x	A FIRST preliminary amendment.				
14.	A SECOND or SUBSEQUENT preliminary amendment.				
15. x	A substitute specification.				
16.	A change of power of attorney and/or address letter.				
17.	A computer-readable form of the sequence listing in accordance with PCT Rule 13ter.2 and 35 U.S.C. 1.821 - 1.825.				
18. x	A second copy of the published international application under 35 U.S.C. 154(d)(4).				
19.	A second copy of the English language translation of the international ap	plication under 35 U.S.C. 154(d)(4).			
20. x	Other items or information Substitute Abstract, Marked-up copy of spe Examination Report, Two (2) Sheets of For				

U.S. APPLICATION NO. (if known	see 37 CFR 1.5)	INTERNATIONAL APPLICAT			
<u> 10/0</u>	10179	PCT/SE00	/01257	LAGROTH-028	
17. x The following fees are submitted:				CALCULATIONS P	TO USE ONLY
BASIC NATIONAL FE					
Neither international preliminary examination fee (37 CFR I 482) nor international search fee (37 CFR I.445(a)(2)) paid to USPTO and International Search Report not prepared by the EPO or JPO \$1040.00					
International preliminary examination fee (37 CFR 1.482) not paid to USPTO but International Search Report prepared by the EPO or JPO \$890 00					
International preliminary examination fee (37 CFR 1 482) not paid to USPTO but international search fee (37 CFR 1 445(a)(2)) paid to USPTO \$740.00					
International preliminary examination fee (37 CFR 1.482) paid to USPTO but all claims did not satisfy provisions of PCT Article 33(1)-(4)\$710.00					
International preliminary examination fee (37 CFR 1.482) paid to USPTO and all claims satisfied provisions of PCT Article 33(1)-(4) \$100.00					
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Processing fee of \$\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20} \text{30 months from the earliest claimed priority date (37 CFR 1.492 (f)). }\frac{1}{20					
TOTAL NATIONAL FEE = \$ 1,04					
Fee for recording the enclosed assignment (37 CFR 1.21 (h)). Assignment					
must be accompanied by appropriate cover sheet (37 CFR 3.28, 3.31) + \$ (per property).					
TOTAL FEES ENCLOSED =			\$ 1,040.00		
*As In Preliminary Amendment				Amount to be Refunded:	s
				Charged:	\$
a. A check in th	e amount of \$	to co	over the above fees	s is enclosed.	
b. x Please charge my Deposit Account No. 12-1095 in the amount of S 1,040.00					
to cover the above fees. A duplicate copy of this sheet is enclosed.					
c. X The Commissioner is hereby authorized to charge any additional fees which may be required or credit any overpayment to my Deposit Account No. 12-1095. A duplicate copy of this sheet is enclosed.					
NOTE: Where an appropriate time limit under 37 CFR 1.494 or 1.495 has not been met, a petition to revive					
(37 CFR 1.137 (a) or (b)) must be filed and granted to restore the application to pending status.					
SEND ALL CORRESPOND		-			
Arnold H. Krumholz	Arnold H. Krumholz SIGNATURE				
LERNER, DAVID, LITTENBERG, KRUMHOLZ & MENTLIK, LLP 600 South Avenue West Westfield, New Jersey 07090				Arnold H. Krumholz	
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PATENT LAGROTH 3.3-028

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re Patent Application of

Hans-Olof BACKLUND

Group Art Unit:

International Application No.

PCT/SE00/01257

Examiner:

International Filing Date:

15 June 2000

Date: December 12, 2001

For: A METHOD AND MEANS FOR MEASURING

STRESS FORCES IN REFINERS

X

Commissioner for Patents Washington, D.C. 20231

PRELIMINARY AMENDMENT

Sir:

Preliminary to initiation of the prosecution of the above-identified pending U.S. patent application, the following amendments and remarks are respectfully submitted.

IN THE ABSTRACT

Please delete the Abstract as filed and substitute therefor the attached revised Abstract.

IN THE SPECIFICATION

Please amend the Specification in accordance with the attached revised Specification.

IN THE CLAIMS

Please cancel claims 1-13 and add new claims 14-28.

14. (NEW) A method of measuring the stress forces in a refining disk having a refining surface including a plurality of refiner bars and employed in a refiner including a pair of refiner disks defining a refining gap therebetween, said method comprising providing a measuring surface comprising at least a portion of a plurality of said refiner bars, resiliently mounting said measuring surface in said refiner surface, and measuring said stress forces across said measuring surface.

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- of claim 14 wherein method (NEW) The surface mounting of said measuring comprises resilient resiliently journaling said measuring surface in a direction substantially parallel to said refining surface whereby said measuring surface is movable in said direction in response to a stress force with respect to a permanent force sensor connected to said measuring surface.
- 16. (NEW) The method of claim 14 including calculating the size and distribution of the output transferred to material passing through said refining gap based on said stress force measured by said measuring surface, and employing said calculation to control the refining process.
- 17. (NEW) Apparatus for measuring stress forces in a refining disk having a refining surface including a plurality of refiner bars utilized in connection with a pair of refining disks defining a refining gap therebetween, comprising at least one measuring member disposed on said refiner surface and including a measuring surface including at least a portion of a plurality of said refiner bars, and resilient mounting means for resiliently mounting said at least one measuring member on said refiner surface.
- 18. (NEW) The apparatus of claim 17 wherein said at least one measuring member comprises a plurality of measuring members.
- 19. (NEW) The apparatus of claim 17 wherein said at least one measuring member comprises a force sensor and a measuring body connecting said force sensor to said measuring surface.
- 20. (NEW) The apparatus of claim 19 wherein said force sensor is in abutment with said measuring body, and including attachment means for fixing said force sensor with respect to said measuring body.
- 21. (NEW) The apparatus of claim 20 wherein said resilient mounting means comprises mounting means for resiliently journaling said measuring surface in a direction substantially parallel to said refiner surface.

- 22. (NEW) The apparatus of claim 21 wherein said measuring surface is connected to said measuring body, and said measuring body extends from said measuring surface on the side of said force sensor so as to provide a measuring body extension, said measuring body extension including a joint portion where said measuring body is movable in a direction substantially parallel to said refiner surface.
- 23. (NEW) The apparatus of claim 22 wherein said measuring body has a substantially circular cross-section, and wherein said joint portion comprises a flattened portion of said measuring body disposed below said force sensor.
- 24. (NEW) The apparatus of claim 19 wherein said force sensor comprises a piezoelectric sensor.
- 25. (NEW) The apparatus of claim 17 wherein said resilient mounting means comprises a sealing member surrounding said measuring surface for joining said measuring surface to said refiner surface.
- 26. (NEW) The apparatus of claim 25 wherein said sealing member comprises a yieldable material.
- 27. (NEW) The apparatus of claim 26 including a casing surrounding said force sensor and said measuring body, said attachment means attaching said force sensor to said casing, said measuring body including a first end and a second end, said first end of said measuring body attached to said casing and said second end of said measuring body attached to said measuring surface, said measuring surface and said sealing member closing said casing.
- 28. (NEW) The apparatus of claim 27 including a sleeve enclosing said sealing means, whereby said sleeve, said sealing means and said measuring surface are inserted in said casing when said casing is sealed.

REMARKS

The above-noted cancellation of claims 1-13, and addition of new claims 14-28, as well as the submission of a new Abstract and revisions to the Specification, are respectfully

Application No. PCT/SE00/01257

submitted prior to initiation of the prosecution of this application in the U.S. Patent and Trademark Office.

The above-noted new claims are respectfully submitted in order to more clearly and appropriately claim the subject matter which applicants consider to constitute their inventive contribution. No new matter is included in these amendments. In addition, the revisions to the Abstract and Specification are submitted in order to clarify and correct the Abstract and Specification and to conform them to all of the requirements of U.S. practice. No new matter is included in these amendments.

In view of the above, it is respectfully requested that these amendments now be entered, and that prosecution on the merits of this application now be initiated. If, however, for any reason the Examiner does not believe such action can be taken, it is respectfully requested that he telephone applicant's attorney at (908) 654-5000 in order to overcome any objections which he may have.

If there are any additional charges in connection with this requested amendment, the Examiner is authorized to charge applicant's Deposit Account No. 12-1095 therefor.

Respectfully submitted,

LERNER, DAVID, LITTENBERG, KRUMHOLZ & MENTLIK, LLP

ARNOLD H. KRUMHOLZ Reg. No. 25,428

600 South Avenue West Westfield, NJ 07090-1497 Telephone: (908) 654-5000 Facsimile: (908) 654-7866

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A METHOD AND MEANS FOR MEASURING STRESS FORCES IN REFINERS FIELD OF THE INVENTION

[0001] The present invention relates to a method and a measuring device for measuring stress forces in refiners having refining discs that between them define a refining gap for refining material.

BACKGROUND OF THE INVENTION

above are used for refining material containing fiber. The refiner generally comprises refining members in the form of discs disks which rotate in relation to each other and between which the material for refining passes from the inner periphery of the refining members, where the material is supplied, to the outer periphery of the refining members, through a refining gap formed between the refining members. Often one of the refining discs disks is fixed whereas the other rotates. The refining discs disks are generally constructed from segments provided with bars on their surface. The inner segments can then have a coarser pattern and the outer segments a finer pattern in order to produce fine refining of the material.

[0003] To ensure high quality when refining material containing fiber, the disturbances in operating conditions that continually occur for various reasons must be corrected by constant control of the various refining parameters to optimum values. This can be achieved by altering the supply of water, for instance, so that a larger or smaller cooling effect is obtained, by changing the flow of material for refining, by adjusting the distance between the refining members, or by a combination of these measures. Accurate determination of the energy transferred to the material for refining, and also of the distribution of the energy over the surface of the refining members, are necessary to enable the necessary adjustments and corrections to be performed.

[0004] To determine the energy/output transferred to the material for refining, it is already known to try to measure

the shear forces appearing in the refining zone. What is known as a shear force occurs when two surfaces move in relation to each other with a viscous liquid between the surfaces. Such a shear force is also created in a refiner used for refining wood chips mixed with water. It may be imagined that the chips of wood are both sheared and rolled between the refining discs, as well as colliding with each other and with the bars. The shear force is caused, inter alia, by the combined force of the discs and by the friction coefficient of friction. The normal force exerted on the surface also varies with the radius.

In through SE-C-504801 As shown in Swedish Patent Application No. 504,801, a measuring device is already known comprising a special sensor bar, i.e. a bar provided with sensors which sense the load exerted on the sensor bar during refining, at a number of measuring points along the bar. However, the drawback of this arrangement is that measuring is only performed on occasional bars, and the result is therefore unreliable. Furthermore, the type of transducer, or strain gauge, used in bar experiments have a short service life since the transducers are located close to the refining surface and the material used to screen the transducers from steam and pulp is subjected to an extremely demanding environment. However, despite these drawbacks, strain gauges must be used because of the design of this measuring device.

[0006] The One object of the present invention is to solve the problems mentioned above and, first of all, to provide a method and a measuring device that produces a more reliable result than previously known devices, and also to provide a device with potential for a longer service life than previously known devices, thus making it more economical.

This object is achieved by a method as defined in claim 1 and with the characteristics specified therein, and also with a measuring device as defined in claim 4.

SUMMARY OF THE INVENTION

In accordance with the present invention, these and [0007] other objects have now been realized by the invention of a method of measuring the stress forces in a refining disk having a refining surface including a plurality of refiner bars and employed in a refiner including a pair of refiner disks defining a refining gap therebetween, the method comprising providing a measuring surface comprising at least a portion of a plurality of the refiner bars, resiliently mounting the measuring surface in the refiner surface, and measuring the stress forces across the measuring surface. Preferably, the resilient mounting of the measuring surface comprises resiliently journaling the measuring surface in a direction substantially parallel to the refining surface whereby the measuring surface is movable in the direction in response to a stress force with respect to a permanent force sensor connected to the measuring surface.

[0008] In accordance with one embodiment of the method of the present invention, the method includes calculating the size and distribution of the output transferred to material passing through the refining gap based on the stress force measured by the measuring surface, and employing the calculation to control the refining process.

In accordance with the present invention, apparatus has also been discovered for measuring stress forces in a refining disk having a refining surface including a plurality of refiner bars utilized in connection with a pair of refining disks defining a refining gap therebetween, comprising at least one measuring member disposed on the refiner surface and including a measuring surface including at least a portion of a plurality of the refiner bars, and resilient mounting means for resiliently mounting the at least one measuring member on the refiner surface. Preferably, the at least one measuring member comprises a plurality of measuring members.

[0010] In accordance with one embodiment of the apparatus of the present invention, the at least one measuring member

comprises a force sensor and a measuring body connecting the force sensor to the measuring surface. Preferably, the force sensor is in abutment with the measuring body, and the apparatus includes attachment means for fixing the force sensor with respect to the measuring body. Preferably, the resilient mounting means comprises mounting means for resiliently journaling the measuring surface in a direction substantially parallel to the refiner surface.

In accordance with another embodiment of the apparatus of the present invention, the measuring surface is connected to the measuring body, and the measuring body extends from the measuring surface on the side of the force sensor so as to provide a measuring body extension, the measuring body extension including a joint portion where the measuring body is movable in a direction substantially parallel to the refiner surface. Preferably, the measuring body has a substantially circular cross-section, and the joint portion comprises a flattened portion of the measuring body disposed below the force sensor.

[0012] In accordance with one embodiment of the apparatus of the present invention, the force sensor comprises a piezoelectric sensor.

[0013] In accordance with another embodiment of the apparatus of the present invention, the resilient mounting means comprises a sealing member surrounding the measuring surface for joining the measuring surface to the refiner surface. Preferably, the sealing member comprises a yieldable material. In a preferred embodiment, the apparatus includes a casing surrounding the force sensor and the measuring body, the attachment means attaching the force sensor to the casing, the measuring body including a first end and a second end, the first end of the measuring body attached to the casing and the second end of the measuring body attached to the measuring surface, the measuring surface and the sealing member closing the casing. In a preferred embodiment, the apparatus includes a sleeve enclosing the sealing means, whereby the sleeve, the

sealing means and the measuring surface are inserted in the casing when the casing is sealed.

The According to the method is thus characterised in that—of the present invention, measurement of the force stress is performed across a measuring surface constituting a part of a refining discdisk, said the measuring surface comprising at least parts of more than one bar and being resiliently mounted in relation to the surface of the refining—disc disk. measuring device is provided with corresponding means for performing the method. The present invention thus reveals the comparison with known advantage that, in technology, measurement of the stress force is performed over a relatively large surface, thereby producing a considerably more reliable result.

[0015] According to a preferred embodiment of the present invention, measurement is performed by the measuring surface being resiliently journalled in a direction parallel with the surface of the refining disc disk and being movable in said direction in the event of a stress force, in relation to a rigidly mounted force sensor with which the measuring surface is connected, said the force sensor thus being influenced by and measuring said the stress force. The measuring device in turn reveals features comprising equivalent members.

[0016] According to a particularly preferred feature of the present invention, therefore, the measuring device comprises a force sensor and a body connecting the sensor with the measuring surface. Through this arrangement the present invention achieves the advantage that the force stress is measured directly, instead of indirectly by measurement of linear strain and the like, as occurs with known technology.

[0017] The sensor, which is preferably a piezoelectric force sensor constructed of quartz crystal (a "quartz sensor") also contributes to an extremely rigid measuring device being possible. The preferred sensor will withstand temperatures of up to about 200°C and is also linear up to this temperature.

[0018] In accordance with another preferred feature of the present invention, the measuring surface is connected to said the body and the part of said—the body that extends on the side of the force sensor opposite to the measuring surface, is provided with a joint where the body is movable in a direction substantially parallel with the surface of the refining disc disk. However, as mentioned above, since the force sensor has a relatively stiff spring action, the shear forces will only cause extremely small movements in the joint, and thus the measuring device. This makes it easier to seal the measuring device against steam and wood chips penetrating from the surroundings, neither will it be as sensitive to material that accumulates around the measuring device. These are important In the direction advantages over the known technology. perpendicular to the measuring surface, the body has such a high degree of rigidity that no changes will occur in the refining gap, which is another advantage.

Additional advantages and features of the invention are revealed in the sub-claims.

The present invention will now be described with reference to the embodiment illustrated in the accompanying drawings, in which

Figure 1 shows a view in perspective of a refining segment forming part of a refining disc, provided with measuring devices in accordance with the present invention;

Figure 2 shows a basic layout sketch of a measuring device in accordance with the present invention;

Figures 3a and 3b illustrate the force ratio applicable for the invention; and

Figure 4 shows a view, partly in section, of a measuring device in accordance with the present invention.

BRIEF DESCRIPTION OF THE DRAWINGS

[0019] The present invention will now be more fully described with reference to the following detailed description which, in turn, refers to the accompanying drawings, in which:

- [0020] Figure 1 is a front, perspective view of a refining segment forming part of a refining disk provided with measuring devices in accordance with the present invention;
- [0021] Figure 2 is a side, elevational, schematic representation of a basic layout of a measuring device in accordance with the present invention;
- [0022] Figure 3a is a schematic representation showing the force ratio applicable to the present invention;
- [0023] Figure 3b is a schematic representation showing the force ratio applicable to the present invention; and
- [0024] Figure 4 is a side, elevational, partially sectional view of a measuring device in accordance with the present invention.

DETAILED DESCRIPTION

Figure 1 thus—illustrates a part of a refining disc disk in the form of a refining segment 1, provided with a pattern comprising a number of bars 3 extending substantially radial direction. Measuring devices 5, in accordance with the present invention, are also illustrated schematically in this figure 1. These measuring devices preferably have a circular measuring surface, with a diameter in—on the order of magnitude of 30 mm, for instance, but the measuring surface may also have a different geometric shape. The measuring devices are preferably arranged at different radial distances from the centre—center of the refining—disc disk, and segments at different distances from the centre center are also preferably provided with measuring devices. It is also advantageous for the measuring devices to be staggered peripherally in relation to each other, all with the object of being able-better able to determine the force distribution in the refiner and thus for better to-control of the refining process. When a measuring device is affected by a force parallel with the surface of the refining discdisk/segment, the force sensor of the measuring device will generate a signal that is proportional to the load.

[0026] The measuring device according to the <u>present</u> invention functions in accordance with the principle illustrated in figure 2. A <u>disc_disk_segment 1</u> can be seen here from the side, equipped with bars 3. A measuring device 5 is also visible, comprising a part of the surface of the <u>disc_disk_segment</u> and being provided with a number of bars 6, or at least parts thereof. When the refining <u>disc_disk_is</u> subjected to a shear load F, the measuring device 5 (the sensor) will take up a load F_m which is denoted by the following expression:

$$F_{\mathbb{M}} = F \cdot \frac{1_1}{1_2} \quad (1)$$

where l is the distance between the point where a sensor 10 in the measuring device is secured and the joint 8 of the device, and where 1 is the distance between the measuring surface 7 of the measuring device and the joint 8. This formula is valid provided the joint does not take up any torque, and that the pressure distribution over the measuring surface 7 subjected to the shear force is not too uneven. The joint 8 consists in principle of a metal sheet of such small thickness so as to give-provide a negligible contribution to the total stiffness of the measuring device, while at the same time being able to withstand the loads to which it is subjected. The thickness of the metal sheet can at the same time be rather large since the sensor itself is relatively rigid, giving little flexure in the sheet. The dimension of the joint 8 shall—is thus be adjusted to withstand the vertical load occurring, while at the same time absorbing only a negligible part of the lateral load that the screw and the sensor shall—absorb. See also the detailed description in conjunction with figure 4.

[0027] The model in figures 3a and 3b describes how high and low rigidity, respectively, affect the function of the measuring device, through the rigidity that sensor, attachment screw (the attachment member by which the sensor is fixed in relation to the measuring surface and the body, see Fig. 4)

and the joint possess. The force and the torque absorbed by the sensor/attachment screw and the joint, respectively, are controlled by the ratio $F_{\rm sensor} = k_2 \cdot \delta$ and $M = k_3 \cdot \Delta \phi$, where M is the torque in the joint. k_2 is in this case the rigidity of the spring 15, that is to say the sensor 10 together with the attachment screw 20, and k_3 is the rigidity of the journaling point/joint 8. The ratio shows clearly that if F = constant and k_2 increases, then δ will decrease, and thus also M, since the torque is directly proportional to the flexure δ for small angles. In the case under discussion k_2 is large and the equation (1) is therefore valid.

[0028] Ιt should be pointed out that, in this relatively high rigidity of the sensor/attachment results in high rigidity in relation to the load that the sensor/screw shall absorbs. The load may vary greatly across the refining zone, e.g. from an order of magnitude of 20N to an order of magnitude of 150N. In the present case, with an estimated average value of about 40N, displacements of the measuring surface are obtained that can be measured hundredths of a millimetremillimeter. As mentioned earlier above, these minor displacements facilitate sealing the device from the surrounding environment. As to for the body 17, this can be considered as completely rigid in the direction perpendicular to the measuring surface.

[0029] Figure 4 shows a preferred embodiment of a measuring device in accordance with the present invention. The measuring device 5 comprises a measuring surface 7 provided with bars 6, or parts of bars, which measuring surface constitutes a part of a disc disk segment as illustrated in figure 1. As can also be seen in figure 1, the measuring device has a preferably has a circular measuring surface.

[0030] The measuring surface 7 is in direct contact with a body 17, preferably of steel, extending inside the device. The measuring surface is preferably screwed to the body 17. Slightly below the measuring surface the body 17 is provided

with a transverse recess in which a force sensor 10 is arranged, preferably a quartz sensor. Here, too, the body 17 is provided with a through hole in which an attachment screw 20 is applied, passing through the hole and securing the sensor 10. The sensor 10 is thus fixed in relation to the body 17 by means of the screw 20, as will be described below. Other attachment means for the sensor 10 are naturally possible. Otherwise, the body 17 preferably has a circular cross section. Further down beneath the sensor, the body 17 assumes a narrowing, flattened shape in an area corresponding to the joint 8, mentioned earlier above, and described in conjunction with figures 2, 3a and 3b.

The sensor 10 and the body 17 are arranged disposed [0031] inside a protective casing 22. This casing has an opening at the top, adjacent to the surrounding refining segment, which is closed by the measuring surface 7, a seal 12 surrounding the measuring surface, and a sleeve 13 in which the seal is arranged disposed. The seal 12 is of a particularly suitable, somewhat yielding material such as rubber, so that it can permit the small movements that the shear forces give rise to in the measuring surface, and still achieve a good seal that prevents steam and pulp from penetrating into the device. The seal preferably has a dampening effect as regards, inter alia, the vibrations that occur during operation. The purpose of the sleeve 13 is primarily to facilitate sealing of the measuring device since the measuring surface and the seal are first assembled in the sleeve which can then easily be inserted partially into the casing 22. Naturally, it is possible to omit the sleeve.

[0032] The casing 22 also has a function in securing the sensor 10 in relation to the measuring surface 7. The sensor is thus secured in the casing by means of the attachment screw 20. Finally, the body 17 is attached in the casing at the end opposite to the measuring surface.

The invention is not limited to the embodiment illustrated in the drawings. It can be modified and altered in many ways

obvious to one skilled in the art, within the scope of the appended claims.

Mith reference to particular embodiments, it is to be understood that these embodiments are merely illustrative of the principles and applications of the present invention. It is therefore to be understood that numerous modifications may be made to the illustrative embodiments and that other arrangements may be devised without departing from the spirit and scope of the present invention as defined by the appended claims.

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10/018126 JC13 Rec'd PCT/FTC 12 DEC 2001

A METHOD AND MEANS FOR MEASURING STRESS FORCES IN REFINERS FIELD OF THE INVENTION

[0001] The present invention relates to a method and a measuring device for measuring stress forces in refiners having refining discs that between them define a refining gap for refining material.

BACKGROUND OF THE INVENTION

[0002] Refiners such as those noted above are used for refining material containing fiber. The refiner generally comprises refining members in the form of disks which rotate in relation to each other and between which the material for refining passes from the inner periphery of the refining members, where the material is supplied, to the outer periphery of the refining members, through a refining gap formed between the refining members. Often one of the refining disks is fixed whereas the other rotates. The refining disks are generally constructed from segments provided with bars on their surface. The inner segments can then have a coarser pattern and the outer segments a finer pattern in order to produce fine refining of the material.

[0003] To ensure high quality when refining material containing fiber, the disturbances in operating conditions that continually occur for various reasons must be corrected by constant control of the various refining parameters to optimum values. This can be achieved by altering the supply of water, for instance, so that a larger or smaller cooling effect is obtained, by changing the flow of material for refining, by adjusting the distance between the refining members, or by a combination of these measures. Accurate determination of the energy transferred to the material for refining, and also of the distribution of the energy over the surface of the refining members, are necessary to enable the necessary adjustments and corrections to be performed.

[0004] To determine the energy/output transferred to the material for refining, it is known to try to measure the shear forces appearing in the refining zone. What is known as a

shear force occurs when two surfaces move in relation to each other with a viscous liquid between the surfaces. Such a shear force is also created in a refiner used for refining wood chips mixed with water. It may be imagined that the chips of wood are both sheared and rolled between the refining discs, as well as colliding with each other and with the bars. The shear force is caused, *inter alia*, by the combined force of the discs and by the coefficient of friction. The normal force exerted on the surface also varies with the radius.

[0005] As shown in Swedish Patent Application No. 504,801, a measuring device is known comprising a special sensor bar, i.e. a bar provided with sensors which sense the load exerted on the sensor bar during refining, at a number of measuring points along the bar. However, the drawback of this arrangement is that measuring is only performed on occasional bars, and the result is therefore unreliable. Furthermore, the type of transducer, or strain gauge, used in bar experiments have a short service life since the transducers are located close to the refining surface and the material used to screen the transducers from steam and pulp is subjected to an extremely demanding environment. However, despite these drawbacks, strain gauges must be used because of the design of this measuring device.

[0006] One object of the present invention is to solve the problems mentioned above and, first of all, to provide a method and a measuring device that produces a more reliable result than previously known devices, and also to provide a device with potential for a longer service life than previously known devices, thus making it more economical.

SUMMARY OF THE INVENTION

[0007] In accordance with the present invention, these and other objects have now been realized by the invention of a method of measuring the stress forces in a refining disk having a refining surface including a plurality of refiner bars and employed in a refiner including a pair of refiner disks defining a refining gap therebetween, the method

comprising providing a measuring surface comprising at least a portion of a plurality of the refiner bars, resiliently mounting the measuring surface in the refiner surface, and measuring the stress forces across the measuring surface. Preferably, the resilient mounting of the measuring surface comprises resiliently journaling the measuring surface in a direction substantially parallel to the refining surface whereby the measuring surface is movable in the direction in response to a stress force with respect to a permanent force sensor connected to the measuring surface.

[0008] In accordance with one embodiment of the method of the present invention, the method includes calculating the size and distribution of the output transferred to material passing through the refining gap based on the stress force measured by the measuring surface, and employing the calculation to control the refining process.

[0009] In accordance with the present invention, apparatus has also been discovered for measuring stress forces in a refining disk having a refining surface including a plurality of refiner bars utilized in connection with a pair of refining disks defining a refining gap therebetween, comprising at least one measuring member disposed on the refiner surface and including a measuring surface including at least a portion of a plurality of the refiner bars, and resilient mounting means for resiliently mounting the at least one measuring member on the refiner surface. Preferably, the at least one measuring member comprises a plurality of measuring members.

[0010] In accordance with one embodiment of the apparatus of the present invention, the at least one measuring member comprises a force sensor and a measuring body connecting the force sensor to the measuring surface. Preferably, the force sensor is in abutment with the measuring body, and the apparatus includes attachment means for fixing the force sensor with respect to the measuring body. Preferably, the resilient mounting means comprises mounting means for

resiliently journaling the measuring surface in a direction substantially parallel to the refiner surface.

[0011] In accordance with another embodiment of the apparatus of the present invention, the measuring surface is connected to the measuring body, and the measuring body extends from the measuring surface on the side of the force sensor so as to provide a measuring body extension, the measuring body extension including a joint portion where the measuring body is movable in a direction substantially parallel to the refiner surface. Preferably, the measuring body has a substantially circular cross-section, and the joint portion comprises a flattened portion of the measuring body disposed below the force sensor.

[0012] In accordance with one embodiment of the apparatus of the present invention, the force sensor comprises a piezoelectric sensor.

accordance with another embodiment of the Ιn [0013] apparatus of the present invention, the resilient mounting means comprises a sealing member surrounding the measuring surface for joining the measuring surface to the refiner surface. Preferably, the sealing member comprises a yieldable material. In a preferred embodiment, the apparatus includes a casing surrounding the force sensor and the measuring body, the attachment means attaching the force sensor to the casing, the measuring body including a first end and a second end, the first end of the measuring body attached to the casing and the second end of the measuring body attached to the measuring surface, the measuring surface and the sealing member closing the casing. In a preferred embodiment, the apparatus includes a sleeve enclosing the sealing means, whereby the sleeve, the sealing means and the measuring surface are inserted in the casing when the casing is sealed.

[0014] According to the method of the present invention, measurement of the force stress is performed across a measuring surface constituting a part of a refining disk, the measuring surface comprising at least parts of more than one bar and

being resiliently mounted in relation to the surface of the refining disk. The measuring device is provided with corresponding means for performing the method. The present invention thus reveals the advantage that, in comparison with known technology, measurement of the stress force is performed over a relatively large surface, thereby producing a considerably more reliable result.

[0015] According to a preferred embodiment of the present invention, measurement is performed by the measuring surface being resiliently journalled in a direction parallel with the surface of the refining disk and being movable in said direction in the event of a stress force, in relation to a rigidly mounted force sensor with which the measuring surface is connected, the force sensor thus being influenced by and measuring the stress force. The measuring device in turn reveals features comprising equivalent members.

[0016] According to a particularly preferred feature of the present invention, the measuring device comprises a force sensor and a body connecting the sensor with the measuring surface. Through this arrangement the present invention achieves the advantage that the force stress is measured directly, instead of indirectly by measurement of linear strain and the like, as occurs with known technology.

[0017] The sensor, which is preferably a piezoelectric force sensor constructed of quartz crystal (a "quartz sensor") also contributes to an extremely rigid measuring device being possible. The preferred sensor will withstand temperatures of up to about 200°C and is also linear up to this temperature.

[0018] In accordance with another preferred feature of the present invention, the measuring surface is connected to the body and the part of the body that extends on the side of the force sensor opposite to the measuring surface is provided with a joint where the body is movable in a direction substantially parallel with the surface of the refining disk. However, as mentioned above, since the force sensor has a relatively stiff spring action, the shear forces will only cause

extremely small movements in the joint, and thus the measuring device. This makes it easier to seal the measuring device against steam and wood chips penetrating from the surroundings, neither will it be as sensitive to material that accumulates around the measuring device. These are important advantages over the known technology. In the direction perpendicular to the measuring surface, the body has such a high degree of rigidity that no changes will occur in the refining gap, which is another advantage.

BRIEF DESCRIPTION OF THE DRAWINGS

[0019] The present invention will now be more fully described with reference to the following detailed description which, in turn, refers to the accompanying drawings, in which:

[0020] Figure 1 is a front, perspective view of a refining segment forming part of a refining disk provided with measuring devices in accordance with the present invention;

[0021] Figure 2 is a side, elevational, schematic representation of a basic layout of a measuring device in accordance with the present invention;

[0022] Figure 3a is a schematic representation showing the force ratio applicable to the present invention;

[0023] Figure 3b is a schematic representation showing the force ratio applicable to the present invention; and

[0024] Figure 4 is a side, elevational, partially sectional view of a measuring device in accordance with the present invention.

DETAILED DESCRIPTION

[0025] Figure 1 illustrates a part of a refining disk in the form of a refining segment 1, provided with a pattern comprising a number of bars 3 extending in a substantially radial direction. Measuring devices 5, in accordance with the present invention, are also illustrated schematically in figure 1. These measuring devices preferably have a circular measuring surface, with a diameter on the order of magnitude of 30 mm, for instance, but the measuring surface may also have a different geometric shape. The measuring devices are preferably

arranged at different radial distances from the center of the refining disk, and segments at different distances from the center are also preferably provided with measuring devices. It is also advantageous for the measuring devices to be staggered peripherally in relation to each other, all with the object of being better able to determine the force distribution in the refiner and thus for better control of the refining process. When a measuring device is affected by a force parallel with the surface of the refining disk/segment, the force sensor of the measuring device will generate a signal that is proportional to the load.

[0026] The measuring device according to the present invention functions in accordance with the principle illustrated in figure 2. A disk segment 1 can be seen here from the side, equipped with bars 3. A measuring device 5 is also visible, comprising a part of the surface of the disk segment and being provided with a number of bars 6, or at least parts thereof. When the refining disk is subjected to a shear load F, the measuring device 5 (the sensor) will take up a load Fm which is denoted by the following expression:

$$F_{m} = F \cdot \frac{1_{1}}{1_{2}}$$
 (1)

where l_2 is the distance between the point where a sensor 10 in the measuring device is secured and the joint 8 of the device, and where l_1 is the distance between the measuring surface 7 of the measuring device and the joint 8. This formula is valid provided the joint does not take up any torque, and that the pressure distribution over the measuring surface 7 subjected to the shear force is not too uneven. The joint 8 consists in principle of a metal sheet of such small thickness so as to provide a negligible contribution to the total stiffness of the measuring device, while at the same time being able to withstand the loads to which it is subjected. The thickness of the metal sheet can at the same time be rather large since the sensor itself is relatively rigid, giving little flexure in

the sheet. The dimension of the joint 8 is thus adjusted to withstand the vertical load occurring, while at the same time absorbing only a negligible part of the lateral load that the screw and the sensor absorb. See also the detailed description in conjunction with figure 4.

The model in figures 3a and 3b describes how high and low rigidity, respectively, affect the function of the measuring device, through the rigidity that sensor, attachment screw (the attachment member by which the sensor is fixed in relation to the measuring surface and the body, see Fig. 4) and the joint possess. The force and the torque absorbed by the sensor/attachment screw and the joint, respectively, are controlled by the ratio $F_{sensor} = k_2 \cdot \delta$ and $M = k_3 \cdot \Delta \phi$, where M is the torque in the joint. k, is in this case the rigidity of the spring 15, that is to say the sensor 10 together with the attachment screw 20, and k, is the rigidity of the journaling point/joint 8. The ratio shows clearly that if F = constant and k_2 increases, then δ will decrease, and thus also M, since the torque is directly proportional to the flexure δ for small angles. In the case under discussion k2 is large and the equation (1) is therefore valid.

[0028] It should be pointed out that, in this case, relatively high rigidity of the sensor/attachment screw results in high rigidity in relation to the load that the sensor/screw absorbs. The load may vary greatly across the refining zone, e.g. from an order of magnitude of 20N to an order of magnitude of 150N. In the present case, with an estimated average value of about 40N, displacements of the measuring surface are obtained that can be measured in hundredths of a millimeter. As mentioned above, these minor displacements facilitate sealing the device from the surrounding environment. As for the body 17, this can be considered as completely rigid in the direction perpendicular to the measuring surface.

[0029] Figure 4 shows a preferred embodiment of a measuring device in accordance with the present invention. The measuring

device 5 comprises a measuring surface 7 provided with bars 6, or parts of bars, which measuring surface constitutes a part of a disk segment as illustrated in figure 1. As can also be seen in figure 1, the measuring device preferably has a circular measuring surface.

The measuring surface 7 is in direct contact with a body 17, preferably of steel, extending inside the device. The measuring surface is preferably screwed to the body 17. Slightly below the measuring surface the body 17 is provided with a transverse recess in which a force sensor 10 is arranged, preferably a quartz sensor. Here, too, the body 17 is provided with a through hole in which an attachment screw 20 is applied, passing through the hole and securing the sensor 10. The sensor 10 is thus fixed in relation to the body 17 by means of the screw 20, as will be described below. Other attachment means for the sensor 10 are possible. Otherwise, the body 17 preferably has a circular cross section. Further down beneath the sensor, the body 17 assumes a narrowing, flattened shape in an area corresponding to the joint 8, mentioned above, and described in conjunction with figures 2, 3a and 3b. The sensor 10 and the body 17 are disposed inside a protective casing 22. This casing has an opening at the top, adjacent to the surrounding refining segment, which is closed by the measuring surface 7, a seal 12 surrounding the measuring surface, and a sleeve 13 in which the seal is disposed. The seal 12 is of a particularly suitable, somewhat yielding material such as rubber, so that it can permit the small movements that the shear forces give rise to in the measuring surface, and still achieve a good seal that prevents steam and pulp from penetrating into the device. The seal preferably has a dampening effect as regards, inter alia, the vibrations that occur during operation. The purpose of the sleeve 13 is primarily to facilitate sealing of the measuring device since the measuring surface and the seal are first assembled in the sleeve which can then easily be inserted partially into the casing 22. Naturally, it is possible to omit the sleeve.

[0032] The casing 22 also has a function in securing the sensor 10 in relation to the measuring surface 7. The sensor is thus secured in the casing by means of the attachment screw 20. Finally, the body 17 is attached in the casing at the end opposite to the measuring surface.

[0033] Although the invention herein has been described with reference to particular embodiments, it is to be understood that these embodiments are merely illustrative of the principles and applications of the present invention. It is therefore to be understood that numerous modifications may be made to the illustrative embodiments and that other arrangements may be devised without departing from the spirit and scope of the present invention as defined by the appended claims.

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ABSTRACT OF THE DISCLOSURE

Methods and apparatus for measuring the stress forces in refining disks are disclosed. The method includes providing a measuring surface comprising at least a portion of a plurality of refiner bars on the refining surface of a refining disk, resiliently mounting the measuring surface in the refiner surface, and measuring the stress forces across the measuring surface.

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A METHOD AND MEANS FOR MEASURING STRESS FORCES IN REFINERS

The present invention relates to a method and a measuring device for measuring stress forces in refiners having refining discs that between them define a refining gap for refining material.

Such refiners are using for refining material containing fiber. The refiner generally comprises refining members in the form of discs which rotate in relation to each other and between which the material for refining passes from the inner periphery of the refining members, where the material is supplied, to the outer periphery of the refining members, through a refining gap formed between the refining members. Often one of the refining discs is fixed whereas the other rotates. The refining discs are generally constructed from segments provided with bars. The inner segments then have a coarser pattern and the outer segments a finer pattern in order to produce fine refining of the material.

To ensure high quality when refining material containing fiber, the disturbances in operating conditions that continually occur for various reasons must be corrected by constant control of the various refining parameters to optimum values. This can be achieved by altering the supply of water, for instance, so that a larger or smaller cooling effect is obtained, by changing the flow of material for refining, by adjusting the distance between the refining members, or a combination of these measures. Accurate determination of the energy transferred to the material for refining, and also of the distribution of the energy over the surface of the refining members, are necessary to enable the necessary adjustments and corrections to be performed.

To determine the energy/output transferred to the material for refining, it is already known to try to measure the shear forces appearing in the refining zone. What is known as a shear force occurs when two surfaces move in relation to each other with a viscous liquid between the surfaces. Such a shear force is also created in a refiner used for refining wood chips mixed with water. It may be imagined that the chips of wood are both sheared and rolled between the refining discs, as well as colliding with each other and the bars. The shear force is caused, inter alia, by the combined force of the discs and by the friction coefficient. The normal force exerted on the surface also varies with the radius.

Through SE-C-504801 a measuring device is already known comprising a special sensor bar, i.e. a bar provided with sensors which sense the load exerted on the sensor bar during refining, at a number of measuring points along the bar. However, the drawback of this arrangement is that measuring is only performed on occasional bars and the result is therefore unreliable. Furthermore, the type of transducer, strain gauge, used in bar experiments have a short service life since

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the transducers are located close to the refining surface and the material used to screen the transducers from steam and pulp is subjected to an extremely demanding environment. However, despite these drawbacks, strain gauges must be used because of the design of this measuring device.

The object of the present invention is to solve the problems mentioned above and, first of all, to provide a method and a measuring device that produces a more reliable result than previously known devices, and also to provide a device with potential for a longer service life than previously known devices, thus making it more economical.

This object is achieved by a method as defined in claim 1 and with the characteristics specified therein, and also with a measuring device as defined in claim 4.

The method is thus characterised in that measurement of the force stress is performed across a measuring surface constituting a part of a refining disc, said measuring surface comprising at least parts of more than one bar and being resiliently mounted in relation to the surface of the refining disc. The measuring device is provided with corresponding means for performing the method. The present invention thus reveals the advantage that, in comparison with known technology, measurement of the stress force is performed over a relatively large surface, thereby producing a considerably more reliable result.

According to a preferred embodiment, measurement is performed by the measuring surface being resiliently journalled in a direction parallel with the surface of the refining disc and being movable in said direction in the event of a stress force, in relation to a rigidly mounted force sensor with which the measuring surface is connected, said force sensor thus being influenced by and measuring said stress force. The measuring device in turn reveals features comprising equivalent members.

According to a particularly preferred feature, therefore, the measuring device comprises a force sensor and a body connecting the sensor with the measuring surface. Through this arrangement the present invention achieves the advantage that the force stress is measured directly, instead of indirectly by measurement of linear strain and the like, as occurs with known technology.

The sensor, which is preferably a piezoelectric force sensor constructed of quartz crystal (a "quartz sensor") also contributes to an extremely rigid measuring device being possible. The preferred sensor will withstand temperatures of up to 200°C and is also linear up to this temperature.

In accordance with another preferred feature, the measuring surface is connected to said body and the part of said body that extends on the side of the

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force sensor opposite to the measuring surface, is provided with a joint where the body is movable in a direction substantially parallel with the surface of the refining disc. However, as mentioned above, since the force sensor has a relatively stiff spring action, the shear forces will only cause extremely small movements in the joint, and thus the measuring device. This makes it easier to seal the measuring device against steam and wood chips penetrating from the surroundings, neither will it be as sensitive to material that accumulates around the measuring device. These are important advantages over the known technology. In the direction perpendicular to the measuring surface, the body has such a high degree of rigidity that no changes will occur in the refining gap, which is another advantage.

Additional advantages and features of the invention are revealed in the sub-claims.

The present invention will now be described with reference to the embodiment illustrated in the accompanying drawings, in which

Figure 1 shows a view in perspective of a refining segment forming part of a refining disc, provided with measuring devices in accordance with the present invention;

Figure 2 shows a basic layout sketch of a measuring device in accordance with the present invention;

Figures 3a and 3b illustrate the force ratio applicable for the invention; and shows a view, partly in section, of a measuring device in accordance with the present invention.

Figure 1 thus illustrates a part of a refining disc in the form of a refining segment 1, provided with a pattern comprising a number of bars 3 extending in substantially radial direction. Measuring devices 5, in accordance with the present invention, are also illustrated schematically in this figure. These measuring devices preferably have a circular measuring surface, with a diameter in the order of magnitude of 30 mm, for instance, but the measuring surface may also have a different geometric shape. The measuring devices are preferably arranged at different radial distances from the centre of the refining disc, and segments at different distances from the centre are also preferably provided with measuring devices. It is also advantageous for the measuring devices to be staggered peripherally in relation to each other, all with the object of being able better to determine the force distribution in the refiner and thus better to control the refining process. When a measuring device is affected by a force parallel with the surface of the refining disc/segment, the force sensor of the measuring device will generate a signal that is proportional to the load.

The measuring device according to the invention functions in accordance with the principle illustrated in figure 2. A disc segment 1 can be seen here from

the side, equipped with bars 3. A measuring device 5 is also visible, comprising a part of the surface of the disc segment and being provided with a number of bars 6, or at least parts thereof. When the refining disc is subjected to a shear load F, the measuring device 5 (the sensor) will take up a load F_m which is denoted by the following expression:

$$F_{m} = F .$$
 (1)

where I_2 is the distance between the point where a sensor 10 in the measuring device is secured and the joint 8 of the device, and where I_1 is the distance between the measuring surface 7 of the measuring device and the joint 8. This formula is valid provided the joint does not take up any torque, and that the pressure distribution over the measuring surface 7 subjected to the shear force is not too uneven. The joint 8 consists in principle of a metal sheet of such small thickness as to give a negligible contribution to the total stiffness of the measuring device while at the same time being able to withstand the loads to which it is subjected. The thickness of the metal sheet can at the same time be rather large since the sensor itself is relatively rigid, giving little flexure in the sheet. The dimension of the joint 8 shall thus be adjusted to withstand the vertical load occurring, while at the same time absorbing only a negligible part of the lateral load that the screw and the sensor shall absorb. See also the detailed description in conjunction with figure 4.

The model in figures 3a and 3b describes how high and low rigidity, respectively, affect the function of the measuring device, through the rigidity that sensor, attachment screw (the attachment member by which the sensor is fixed in relation to the measuring surface and the body, see Fig. 4) and joint possess. The force and the torque absorbed by the sensor/attachment screw and the joint, respectively, are controlled by the ratio Fsensor = $k_2 \cdot \delta$ and M = $k_3 \cdot \Delta \phi$, where M is the torque in the joint. k_2 is in this case the rigidity of the spring 15, that is to say the sensor 10 together with the attachment screw 20, and k_3 is the rigidity of the journalling point/joint 8. The ratio shows clearly that if F = constant and k_2 increases, then δ will decrease, and thus also M since the torque is directly proportional to the flexure δ for small angles. In the case under discussion k_2 is large and the equation (1) is therefore valid.

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It should be pointed out that, in this case, relatively high rigidity of the sensor/attachment screw results in high rigidity in relation to the load that the sensor/screw shall absorb. The load may vary greatly across the refining zone, e.g. from an order of magnitude of 20N to an order of magnitude of 150N. In the present case, with an estimated average value of about 40N, displacements of the measuring surface are obtained that can be measured in hundredths of a millimetre. As mentioned earlier, these minor displacements facilitate sealing the device from the surrounding environment. As to the body 17, this can be considered as completely rigid in the direction perpendicular to the measuring surface.

Figure 4 shows a preferred embodiment of a measuring device in accordance with the present invention. The measuring device 5 comprises a measuring surface 7 provided with bars 6, or parts of bars, which measuring surface constitutes a part of a disc segment as illustrated in figure 1. As can also be seen in figure 1, the measuring device has a preferably circular measuring surface.

The measuring surface 7 is in direct contact with a body 17, preferably of steel, extending inside the device. The measuring surface is preferably screwed to the body 17. Slightly below the measuring surface the body 17 is provided with a transverse recess in which a force sensor 10 is arranged, preferably a quartz sensor. Here, too, the body 17 is provided with a through hole in which an attachment screw 20 is applied, passing through the hole and securing the sensor 10. The sensor 10 is thus fixed in relation to the body 17 by means of the screw 20, as will be described below. Other attachment means for the sensor 10 are naturally possible. Otherwise, the body 17 preferably has a circular cross section. Further down beneath the sensor, the body 17 assumes a narrowing, flattened shape in an area corresponding to the joint 8, mentioned earlier, and described in conjunction with figures 2, 3a and 3b.

The sensor 10 and the body 17 are arranged inside a protective casing 22. This casing has an opening at the top, adjacent to the surrounding refining segment, which is closed by the measuring surface 7, a seal 12 surrounding the measuring surface, and a sleeve 13 in which the seal is arranged. The seal 12 is of a particularly suitable, somewhat yielding material such as rubber, so that it can permit the small movements that the shear forces give rise to in the measuring surface, and still achieve a good seal that prevents steam and pulp from penetrating into the device. The seal preferably has a dampening effect as regards, inter alia, the vibrations that occur during operation. The purpose of the sleeve 13 is primarily to facilitate sealing of the measuring device since the measuring surface and the seal are first assembled in the sleeve which can then easily be inserted partially into the casing 22. Naturally, it is possible to omit the sleeve.

The casing 22 also has a function in securing the sensor 10 in relation to the measuring surface 7. The sensor is thus secured in the casing by means of the attachment screw 20. Finally, the body 17 is attached in the casing at the end opposite to the measuring surface.

The invention is not limited to the embodiment illustrated in the drawings. It can be modified and altered in many ways obvious to one skilled in the art, within the scope of the appended claims.

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CLAIMS

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- 1. A method for measuring stress forces in refiners having refining discs that between them define a refining gap for refining material between bars (3) arranged on the refining discs, **characterized** in that measurement is performed across a measuring surface (7) constituting a part of a refining disc, said measuring surface comprising at least parts of more than one bar (3) and being resiliently mounted in relation to the surface of the refining disc.
- 2. A method as claimed in claim 1, characterized in that measurement is performed by the measuring surface being resiliently journalled in a direction parallel with the surface of the refining disc and being movable in said direction in the event of a stress force, in relation to a permanently inserted force sensor with which the measuring surface is connected, said force sensor thus being influenced by and measuring said stress force.
 - 3. A method as claimed in claim 1 or claim 2, **characterized** in that the size and distribution of the output transferred to the material are calculated on the basis of the measured stress forces and that these calculations are then used to control the refining process.
 - 4. A measuring device for measuring stress forces in refiners comprising refining discs that between them define a refining gap for refining material between bars (3) arranged on the refining discs, **characterized** in that said device comprises members (10) that measure the stress force across a measuring surface (7) constituting a part of a refining disc, in that said measuring surface comprises at least parts of more than one bar (3) and being resiliently mounted in relation to the surface of the refining disc.
- 5. A measuring device as claimed in claim 4, **characterized** in that it comprises a force sensor (10) and a body (17) that connects said sensor to the measuring surface (7).
- 6. A measuring device as claimed in claim 5, **characterized** in that the force sensor (10) abuts said body (17) while at the same time being fixed in relation to said body by means of attachment means (20).

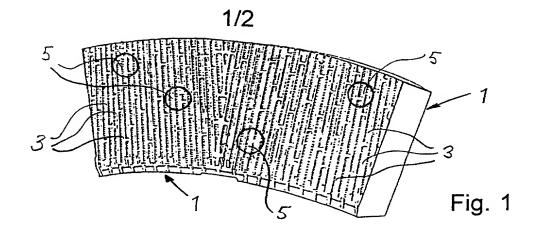
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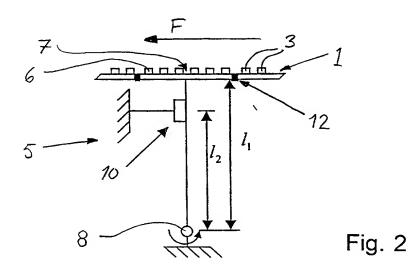
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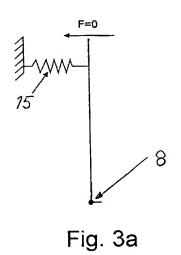
- 7. A measuring device as claimed in claim 6, **characterized** in that it comprises members (12, 17) for resilient journalling of the measuring surface in a direction essentially parallel with the surface of the refining disc.
- 8. A measuring device as claimed in claim 7, **characterized** in that the measuring surface (7) is connected to said body (17) and in that, furthermore, the part of said body that extends on the side of the force sensor (10) opposite to the measuring surface, is provided with a joint (8) where the body is movable in a direction substantially parallel with the surface of the refining disc.

9. A measuring device as claimed in claim 8, **characterized** in that the body (17) is substantially circular in cross section and that the joint (8) is formed by a part of the body, located below the force sensor (10), being flattened.

- 15 10. A measuring device as claimed in any of claims 5-9, **characterized** in that the force sensor (10) is a piezoelectric sensor.
 - 11. A measuring device as claimed in any of claims 4-10, **characterized** in that said measuring surface (7) constitutes a part of the measuring device and that the measuring surface is surrounded by a sealing member (12) by which it is joined to surrounding parts of the measuring device, and which sealing member (12) is made of a somewhat yielding material.
- 12. A measuring device as claimed in claim 11, **characterized** in that it comprises a casing (22), that the force sensor (10) and the body (17) are arranged inside said casing, that the force sensor is attached inside the casing by means of said attachment means (20) and is thus secured in relation to said body, that one end of the body, opposite to the end joined to the measuring surface, is secured in the casing and that the casing is closed by means of the measuring surface (7) and the sealing member (12).
 - 13. A measuring device as claimed in claim 12, **characterized** in that the sealing member is arranged in a sleeve (13) which sleeve, with the sealing member (12) and measuring surface (7), is inserted in the casing (22) in order to seal the casing.







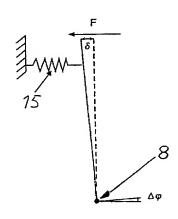


Fig. 3b

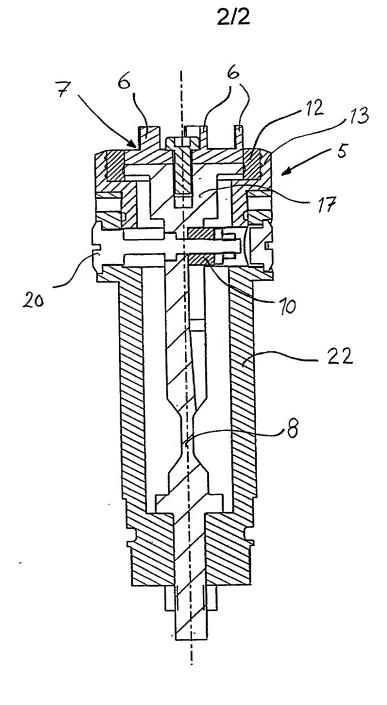


Fig. 4

DECLARATION FOR UTILITY OR DESIGN PATENT APPLICATION

مني .	ATTORNE	Y'S DOCKET NO.: LAGR	OTH-028	
As a below-named inventor, I hereby of My residence, post office address and citiz I believe I am the original, first and sole is are listed below) of the subject matter white	enship are as stated below next to inventor (if only one name is listed to be claimed and for which a pater	i below) or an original, lifst and it is sought on the invention entitle	~4	
A METHOD AND MEANS FOR	MEASURING STRESS I	ORCES IN RECEIVERS		
is attached herete Was filed on 15 Jun Number PCT/SE00/01257	e 2000 as United		(ii applicable).	
I hereby state that I have reviewed and unamendment specifically referred to above.	derstand the contents of the above-	identified specification, including	uie clania, ao america de Company	
I acknowledge the duty to disclose information		lity as defined in Title 37, Code o	of Federal Regulations, § 1.56.	
I hereby claim foreign priority benefits un certificate, or § 365(a) of any PCT intern listed below and have also identified belo having a filing date before that of the appl	der Title 35, United States Code, ational application which designate wany foreign application for pare ication on which priority is claimed	§ 119(a)-(d) of any foreign applic od at least one country other than nt or inventor's certificate, or an	ation(s) for patent or inventor's the United States of America,	
PRIOR FOREIGN APPLICATION(S	5)	DATE OF FILING		
COUNTRY	APPLICATION NUMBER	(month, day, year)	PRIORITY CLAIMED	
⊨ Sweden	9902306-1	17 June 1999	YES 🕅 NO 🗌	
	,		YES NO	
2	, }		YES NO	
LISTING OF FOREIGN APPLICATION	ONS CONTINUED ON PAGE 3 H	iereof 🗌 yes 🖫 no		
I hereby claim the benefit under Title 35,	United States Code, § 119(e) of st	ny United States provisional appli	cation(s) listed below:	
Witness.	Number:	Filing Date:		
Application	Number:	Filing Date:		
I hereby claim the benefit under Title 35, United States Code, §120 of any United States application(s), or § 365(c) of any PCT international application designating the United States of America, listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States or PCT international application in the manner provided by the first paragraph of Title 35. United States Code, § 112. I acknowledge the duty to disclose information which is material to patentability as defined in Title 37. Code of Federal Regulations, § 1.56 which became available between the filing date of the prior application and the national or PCT international filing date of this application:				
U.S. Parent Application Serial Number:	Parent Fil	ing Date:Pa	rent Patent No.:	
U.S. Parent Application Scrial Number: Parent Filing Date: Parent Patent No.:				
PCT Parent Number: Parent Filing Date:				
LISTING OF US APPLICATIONS CONTINUED ON PAGE 3 HEREOF: YES NO				
POWER OF ATTORNEY: As a named to transact all business in the Patent and	Trademark Office connected there	with.		
Lawrence I, Lefner, Reg. No. 18,518; Sidney David, Reg. No. 26,573-Rey H. Wepner, Reg. No. 28,3 No. 32,675 Daniel H. Bobts, Reg. No. 18,684; Peter J. Michael H. Teschner, Reg. No. 32,662 Jeffrey S. Dickey Carravan, Reg. No. 37,592	SO, Stephen B. Goldman, Reg. No. 28,512; Par	ul M. Kochanski, Reg. No. 25,060; Marcus J. A and No. 32 157; Robert B. Cohen, Red. No. 3	2 788- Amold B. Dompieri, Red. Na. 29,796.	
SEND CORRESPONDENCE TO:		DIRECT TELEPHONE CALL	s TO:	
LERNER, DAVID, LITTENBERG	i, Ì	(name and telephone number)		
KRUMHOLZ & MENTLIK		ARNOLD H. KRUMHOLZ		
600 South Avenue West			51 7944	
Westfield New James 07000	i I	(908) 654-5000 Fax: (908) 6	J4-1800	

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DECLARATION - Page 2

ATTORNEY DO	CKET NO	LACROTH-02	9.0
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I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further, that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

ell name of sole or first inventor (given name, family name): Hans-Olof Backlund		
Inventor's signature Homes - Olast Bouchurd		
Residence: Sundsvall, Sweden	Citizenship: Swedish	
Post Office Address: Bagevagen 43 D, S-856 52 Sundsvall		
Full name of second joint inventor, if any (given name, family name): Esko Härl	rönen	
Second Inventor's signature Westerlean	Date 30 Nov. 2001	
Residence: Kajaani, Finland FTX	Citizenship: Finnish	
Post Office Address: Jauhokalliontie 1 E 14, FIN-87200	kajaani, finiand	
Full name of third joint inventor, if any (given name, family name):		
Third Inventor's signature	Date	
Residence:	Citizenshîp:	
Post Office Address:		
Full name of fourth joint inventor, if any (given name, family name): Fourth Inventor's signature		
Residence:		
Bost Office Address:		
Full name of fifth joint inventor (given name, family name):		
Fifth Inventor's signature	Date	
Residence:	Citizenship:	
Post Office Address:		
Full name of sixth joint inventor, if any (given name, family name):		
Sixth Inventor's signature		
Residence:		
Post Office Address:		
Full name of seventh joint inventor, if any (given name, family name):		
Seventh Inventor's signature		
Residence:		
Post Office Address:	- Control of the cont	
Full name of eighth joint inventor, if any (given name, family name):		
Eighth Inventor's signature	Date	
Residence;	Citizenship:	
Post Office Address:		